

# Parametric frequency mixing in the magneto-elastically driven FMR-oscillator

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We demonstrate the nonlinear frequency conversion of ferromagnetic resonance (FMR) frequency by optically excited elastic waves in a thin metallic film on dielectric substrates. Time-resolved probing of the magnetization directly witnesses magneto-elastically driven second harmonic generation, sum- and difference frequency mixing from two distinct frequencies, as well as parametric downconversion of each individual drive frequency. Starting from the Landau-Lifshitz-Gilbert equations, we derive an analytical equation of an elastically driven nonlinear parametric oscillator and show that frequency mixing is dominated by the parametric modulation of FMR frequency.

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Parametric behaviour emerges in a wide range of periodically driven systems when their parameters are also periodically modulated[1]. Examples can be found in nano-optomechanical [2–4] and micro-electromechanical systems [5], (spin) wave dynamics[6], quantum circuitry[7], energy harvesting applications[8], and in line with our current report, magneto-mechanical systems[9] including spin pumping capabilities[10]. The utility of parametric behaviour has been shown for quantum limited detection, noise floor reduction or low noise amplification of small signals[2, 7].

Parametric phenomena in magnetization dynamics have also been extensively studied in the framework of spintronic and magnonic applications[11], where the downconversion of a microwave-driven uniform precession can generate two counter-propagating spin waves of varying frequency and wavevector. The onset of parametric behaviour in these cases is monitored via the enhanced damping and linewidth changes of the ferromagnetic resonance (FMR) precessional motion. Furthermore, time domain probing of FMR precession modulated with multiple microwave electromagnetic fields leads to seeded parametric downconversion[12]. Additional studies along these lines have resulted in the generation and detection of a range of frequency mixing processes of both uniform precessional modes as well as higher energy spin waves[13–15], including frequency up- and down-conversion.

Looking beyond microwave excitation, the overlapping frequency range of (surface) acoustic waves and magnetization precession provides for a unique opportunity to study their interactions and to explore physical processes where coherent elastic deformations could provide the necessary parametric modulation to drive complex magnetization dynamics. In recent years, magnetoelastic interactions have seen a resurgence of interest, and linear coupling between these degrees of freedom have been

demonstrated [16–21]. To our knowledge, only a single report has discussed the potential for nonlinearities in the magnetoelastic interactions[22].

In this report we present experimental evidence for the nonlinear (in the sense of frequency mixing) interaction between multiple coherent elastic deformations and the magnetization precession in a thin ferromagnetic film. To explain our results we perform analytical calculations of the Landau-Lifshitz-Gilbert equation, subject to the periodic excitation of a large amplitude, coherent elastic wave and show that the resulting dynamics can be described by an extended Mathieu equation for a nonlinear parametric oscillator. Simulation results based on our theory show excellent correspondence with experimental results and allow us to identify a range of upconversion responses (enumerated below) as well as the downconverted precessional response commonly associated with parametric modulation.

The enabling feature of the present research is our recent demonstration of a simple optical technique that is able to generate multiple elastic waves utilizing the all-optical ultrafast transient grating (TG) technique[23], which facilitates the excitation and detection of multiple distinct elastic perturbations that propagate along the surface of a magnetic thin film. In our recent reports, we have identified them as the Rayleigh Surface Acoustic Wave (SAW) and the Surface Skimming Longitudinal Wave (SSLW), oscillating at distinct frequencies  $\omega_{SAW}$  and  $\omega_{SSLW}$ . These acoustic transients interact simultaneously with the FMR precession in a nickel film. Varying the applied magnetic field and underlying substrate material allows us to engineer the frequencies and relative elastic excitation strength of the two waves, to experimentally observe sum and difference frequency generation (SHG and DFG at  $\omega_{\pm} = \omega_{SSLW} \pm \omega_{SAW}$ , respectively) and second harmonic generation (SHG, both for  $\omega_{SHG} = \omega_{SAW} + \omega_{SAW}$  and  $\omega_{SHG} = \omega_{SSLW} + \omega_{SSLW}$ ).

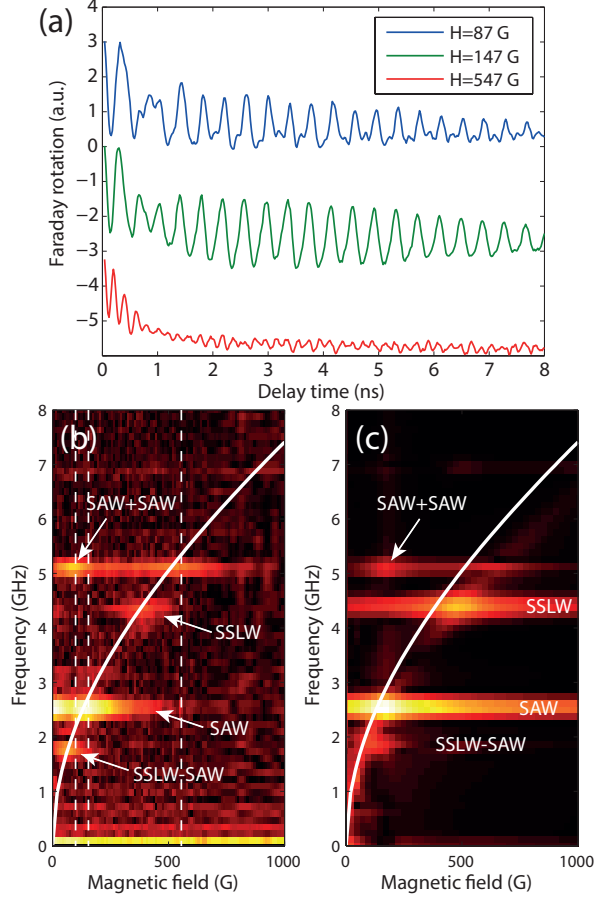


FIG. 1: (a) The time-resolved Faraday rotation for three representative applied fields, exhibiting a range of magnetoelastic responses. (b) The Fourier spectra of Faraday time traces vary strongly with the applied magnetic field, and show maxima when resonant with the elastic driving fields (linear response) as well as at their sum and difference frequencies. Magneto-elastic frequency mixing is observed at the second harmonic frequency of the Rayleigh Surface Acoustic Wave (SAW) and difference frequency with a weaker Surface Skimming Longitudinal Wave (SSLW) wave, (c) The numerical solution of the parametric oscillator equation (Eq. (1)) evidences the same behavior. White solid line marks the FMR-frequency  $\Omega_0(H)/2\pi$ , while vertical dashed lines identify the time traces in (a).

In the TG geometry the sample is excited by two, spatially and temporally coincident optical pulses generating a spatially periodic, instantaneous excitation. Due to thermoelastic mechanisms, large amplitude elastic waves propagate along the surface of the film (as well as into the bulk of the film). A time delayed probe measures the magnetization of the sample based on the rotation of the polarization of the transmitted beam (Faraday configuration), and is sensitive to the out-of-plane component of the magnetization as it precesses under the action of the elastic waves.

As an initial demonstration of magnetoelastic nonlin-

earities, we revisit the Ni/MgO sample configuration we first described in Janusonis et.al. [24]. On this substrate, the TG excitation leads to a strong Rayleigh Surface Acoustic Wave (Rayleigh SAW) and a barely - visible Surface Skimming Longitudinal Wave (SSLW, see e.g.[25]). Figure 1(a) shows the dependence of the magnetization precession amplitude (Faraday rotation, vertically offset) on the magnitude  $H$  of the in-plane applied external magnetic field tilted by angle  $\phi = 30^\circ$  with respect to TG wave vector. The magnetic field allows for tuning the thin - film FMR frequency following the Kittel formula  $\Omega_0 = \gamma\mu_0\sqrt{H(H + M_0)}$ , where  $M_0$  is the saturation magnetization in nickel and  $\gamma$  is the gyromagnetic ratio. For ease of visualization, the spectral amplitude of Fourier transforms of individual scans taken over the entire range of magnetic field are displayed in a 2D map as shown in figure 1(b). Within the range of magnetic field up to 1000 G, the FMR frequency can be tuned to the underlying elastic frequencies (2.55 GHz for SAW and weakly at 4.35 GHz for SSLW), their difference (1.8 GHz) and sum (6.9 GHz) frequencies as well as SAW second harmonic frequency (5.10 GHz). The elastic frequencies are determined by the underlying substrate material and are fixed once a TG period  $\Lambda$  is experimentally selected and shown here for the case of  $\Lambda = 2.2 \mu\text{m}$ . For this combination of metal and substrate, elastic amplitude of SAW is far larger than that of SSLW, resulting in a large precession signal for the linear response at 2.55 GHz and its second harmonic (5.10 GHz), and far weaker sum and difference frequency mixing signals with the weak SSLW. We therefore consider this as a monochromatic elastic wave (SAW) with a small additional contribution of the SSLW.

Theoretical analysis of elastically driven Landau-Lifshitz-Gilbert equations [26] shows that a relatively moderate value of magnetostriction coefficient  $b_1 = 1.5 \times 10^5 \text{ J/m}^3$  in nickel results in a small-angle FMR precession around the external magnetic field (applied in the  $xy$  - plane). The linearization of LLG equations in the vicinity of the equilibrium magnetization direction (see the Supplemental Material for derivation) leads to an equation of a driven parametric oscillator

$$\frac{d^2 m}{dt^2} + \Gamma_0 \frac{dm}{dt} + (\Omega_0^2 + \Omega_1^2 e_{xx}(t))m = F_0 e_{xx}(t) \quad (1)$$

for the in-plane component  $m = M_y(t)/M_0$  of the time-dependent magnetization vector  $\vec{M}(t)$ . The dominant term  $e_{xx}(t)$  of the elastic strain represents a sum of two contributions: a large amplitude, time periodic, SAW excitation at frequency  $\omega_{SAW}$  and a rapidly decaying SSLW excitation in line with our previous Green's function calculation of the elastic response[25].

Equation Eq. (1) represents an approximation of a more complicated equation (Eq. (4) in the Supplemental Material). A detailed analysis shows that the damping term  $\Gamma(t) = \Gamma_0 + \Gamma_1 e_{xx}(t)$  is modulated by

the elastic strain  $e_{xx}(t)$  as well and that there exist high-order nonlinear terms proportional to  $m^2 e_{xx}$  and  $m \frac{dm}{dt} e_{xx}$ . However, the dominant term in the sense of frequency mixing are the parametric modulation of FMR-frequency  $\Omega^2(t) = \Omega_0^2 + \Omega_1^2 e_{xx}(t)$  and the external driving force  $F_0 e_{xx}(t)$ . An intrinsic property of our methodology is that the parametric modulation  $\Omega_1^2(H, \phi) e_{xx}(t) = \frac{\gamma^2 \mu_0 b_1}{M_0} (H + M_0 - [3H + 2M_0] \cos^2 \phi) e_{xx}(t)$  and the external driving force  $F_0(H, \phi) e_{xx}(t) = \frac{\gamma^2 \mu_0 b_2}{2M_0} (H + M_0) \sin 2\phi e_{xx}(t)$  are both proportional to the strain amplitude  $e_{xx}(t)$ . However, their ratio  $F_0/\Omega_1^2 \propto (H + M_0) \sin 2\phi / [H + M_0 - (3H + 2M_0) \cos^2 \phi]$ , which determines the relative strength of parametric modulation to driving force, does not depend on strain and can be adjusted by either changing the magnitude of the applied field,  $H$ , and/or the orientation  $\phi$  of the external magnetic field with respect to TG wave vector.

In figure 1(c), we show the results of the numerical solution of Eq. (1). The solution of the equation results in a time, angle, and field - dependent time trace, which is subsequently Fourier transformed and displayed as a spectral amplitude. In comparison to figure 1(b), we note the exceptional similarity between the experimental data and the calculated response, and in particular the appearance of harmonics of the underlying elastic waves. In the simulation, the SAW and SSLW frequencies are *a posteriori* extracted from the experimental data and the SSLW amplitude and decay time are calculated by the Green's function formalism [23]. The parametrically driven upconversion and downconversion are the results of the simulation.

Figure 2(a) shows the dependence of the Fourier spectra in Fig. 1(b) on the magnetic field at selected frequencies corresponding to the acoustic SAW, and SSLW, as well as the nonlinear responses of SSLW-SAW and SAW+SAW frequencies. The strongest SAW signal displays a resonance at  $H=250$  G. As discussed previously for this material heterostructure, the largest signal corresponds to the SAW excitation which is well approximated by a Lorentzian line shape (dotted line in the figure). In Figure 2(b) we take a closer look at the dependence of SHG signal (SAW+SAW) at 5.10 GHz as a function of the magnetic field, which displays two pronounced maxima corresponding to the  $\Omega_0 = \omega$  and  $\Omega_0 = 2\omega$ , both in the experiment and in the numerical simulation. Here  $\omega$  denotes the frequency of surface acoustic wave. In order to understand the physical origin of this dependence we have applied first-order perturbation theory to Eq. (1) assuming  $e_{xx}(t)$  to be a small parameter. Assuming a monochromatic elastic driving force (SAW only)  $e_{xx}(t) = e_{xx,0} \exp(i\omega t)$  we obtained the following analytical expression for the nonlinear correction at frequency  $2\omega$ :

$$m(2\omega) \propto \frac{1}{\Omega_0^2 - \omega^2 + i\omega\Gamma_0} \frac{\Omega_1^2}{\Omega_0^2 - 4\omega^2 + 2i\omega\Gamma_0}, \quad (2)$$

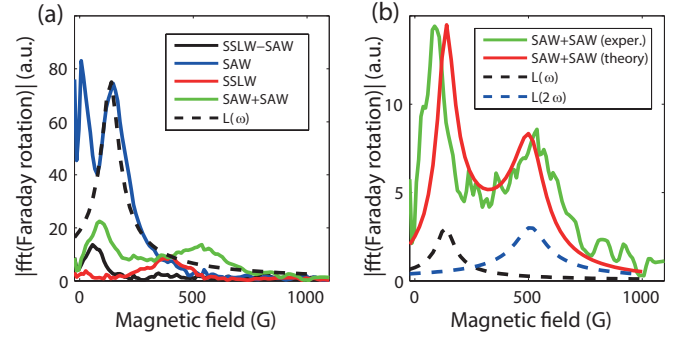


FIG. 2: (a) Horizontal crosssections of experimental (Fig. 1(b)) plots corresponding to SAW and SSLW frequencies as well as their difference (SSLW-SAW) and SAW second harmonic (SAW+SAW) frequencies. The dashed line shows the SAW Lorentzian  $L(\omega)$ . (b) The strongest nonlinear mixing signal (SAW+SAW) is well approximated by an analytical approximation (Eq. (2)); it displays two maxima corresponding to the resonances  $\Omega_0(H = 150 \text{ G}) = \omega$  and  $\Omega_0(H = 520 \text{ G}) = 2\omega$ .

which represents a product of two Lorentzians  $L(\omega)$  and  $L(2\omega)$ . Therefore, in analogy to nonlinear optics[27] the spectral dependence of the second-order susceptibility displays two resonances at frequencies  $\omega$  and  $2\omega$ , respectively. However, whereas in nonlinear optics SHG is caused by  $\chi^{(2)}$ -nonlinearities in the wave equation, in magneto-elasticity it originates from the joint action of the parametric modulation of the FMR frequency and periodic external driving, both at the same frequency  $\omega$ .

The above analytical treatment neglects the second driving frequency at SSLW, which is necessary to explain the sum and difference frequency wave mixing. In contrast to the long-lived SAW, the amplitude of SSLW rapidly decays on a time scale of about 1-3 ns, depending on the elastic constants of the substrate, TG wavelength and nickel thickness. However, replacing the first Lorentzian  $L(\omega)$  in Eq. (2) by a sum of two Lorentzians,  $L(\omega) + L(\omega_{SSLW})$ , allows to approximate the experimental data for SSLW-SAW in Fig. 2(a) as well.

Engineering the elastic properties of the dielectric substrate can be used to enhance existing, or create additional, nonlinear responses. In contrast to the MgO substrate, where the SAW excitation dominates, a similar nickel/glass structure displays markedly different behavior due to the strong contribution of the SSLW excitation[25], providing additional opportunities to tune the nonlinear responsivity. As a demonstration, we perform the same measurements on the Ni/glass structure with a  $1.1 \mu\text{m}$  period, which results in a more efficient magneto-elastic frequency mixing as shown in Figure 3(a). In addition to the linear SAW and SSLW excitations, there now exists two responses at  $\sim 7.83 \text{ GHz}$  and  $\sim 10.20 \text{ GHz}$  which we recognize as the precession response due to the sum frequencies of the underlying elas-

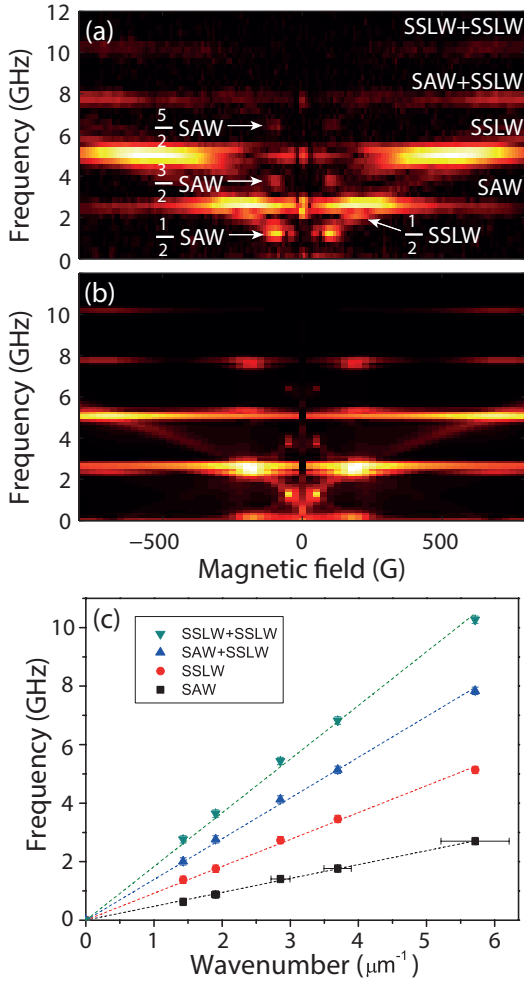


FIG. 3: (a) On glass substrates, two strong elastic waves are generated (SAW and SSLW) allowing the observation of sum frequencies at SAW + SSLW (7.83 GHz) and SSLW + SSLW (10.20 GHz) in addition to the linearly activated precession at 2.73 GHz and 5.10 GHz. Additionally, parametric down-conversion is also witnessed at the half frequency of SAW and SSLW (and their integer multiples). (b) Simulations of the results on glass, where higher strain values can be obtained, show excellent agreement with the experimental findings. (c) Dispersion relations for several grating periodicities. The resultant slope indicates the velocity of the excitation, which for the two lower modes, correspond to the propagation velocity of the underlying elastic waves. For the sum frequencies, the extracted 'velocities' indicate that higher precessional frequencies always occur at sum of the lower elastic responses.

tic waves, SAW + SSLW and SSLW + SSLW (Due to the particularities of the elastic properties of the glass, SAW + SAW excitation overlaps nearly perfectly with the linear SSLW response and is thus not evident.) In addition to these nonlinear sum frequencies, the response on glass is marked by the appearance of precessional amplitude at the parametrically downconverted half frequencies (and their multiples) as indicated in the figure.

Calculations similar to those performed earlier are ac-

complished by adjusting the relative strength of SAW and SSLW for the new configuration. In this case, the time window over which both SAW and SSLW act are unchanged, however, the strength of the excitation is increased for both SAW and SSLW to account for the more favorable elastic constants of the amorphous glass substrate. Under these conditions of strong elastic driving, the simulation is again able to extract the salient features of the experimental findings, in particular, the generation of parametrically downconverted frequencies and the sum frequencies. The data and calculations in Fig. 3(b) demonstrate the effect for a magnetic field angle of  $\phi = 7.5^\circ$  (magnetic field nearly collinear to the TG wavevector), where parametric driving dominates. Likewise, turning the magnetic field angle to larger values suppresses these downconverted and upconverted responses. In the supplemental we show an example of the response at  $\phi = 60^\circ$  where the parametric response is suppressed.

Finally, we aggregate the results of several grating periodicities (1.1, 1.7, 2.2, 3.3 and 4.4  $\mu\text{m}$ ) on the glass substrate, all of which show sum frequency generation, to show the scaling of precessional frequency as a function of grating wavenumber. The extracted velocities for the two lower branches are  $3000 \pm 125$  m/s and  $5900 \pm 110$  m/s in line with our previous measurement and published data for the Rayleigh SAW and longitudinal velocity in glass. For the two upper branches, we extract values of  $8900 \pm 230$  m/s and  $11800 \pm 300$  m/s which overlap, within errors, with the sum frequencies SAW + SSLW and SSLW + SSLW. Velocity values are obtained by zero-intercept linear fits of the dispersion curves, while the horizontal and vertical error bars on the data account for the uncertainty in excitation grating period and frequency uncertainty due to the finite measurement time, respectively. The dispersion relations should be understood in the framework of elastic propagation and the resonant precession that they drive. While the two lower branches represent both elastic velocity and precessional frequency, the upper branches should only be associated with the precession of magnetization at the sum frequencies of the underlying elastic waves.

In summary, we have demonstrated the general feature of parametric excitation of nonlinear magnetization precession under the action of a driving elastic field. Under an applied field, the particularities of the response can be tuned to accentuate or amplify either the sum, difference, or parametric downconverted frequencies. The range of nonlinear responses can be further selected by a careful choice of substrate material, which selects the relative strengths of the active elastic waves. To corroborate our experimental results, we calculate the response of magnetization under the action of elastic waves to arrive at the equation for a parametric oscillator. Numerical and analytical calculations find excellent qualitative agreement to the data. This initial demonstration opens the door

to more complex elastic wave[28] control over magnetization that could herald the emergence of extremely broadband, widely tunable, control of magnetization precession, including magnetization reorientation, and elastic activation of quantized magnonic modes. Furthermore, the presented methodology can be used to investigate novel materials with unknown magneto-elastic properties. Thin films of magnetic MAX-phases with negligible magneto-crystalline anisotropy and possibly high magneto-strictive coupling could be good candidates for future research [29].

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